Electrochemical Reduction of Carbon Dioxide
Fundamentals and Technologies
Jinli Qiao, Yuyu Liu, Jiujun Zhang

Electrode Kinetics of CO Electrodereduction

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# Electrode Kinetics of CO₂ Electroreduction

*Dongmei Sun and Yu Chen*

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## 3.1 INTRODUCTION

Electrochemical reduction of carbon dioxide (ERC) is an attractive way to convert CO₂ because of the following advantages over thermochemical methods: (1) water is the proton source; (2) high equilibrium conversion at ambient temperature; and (3) relatively simple and green [1].

The electrochemical reduction of CO₂ has been studied since the late nineteenth century [2]. In 1904 [3], Coehn and Jahn used zinc, amalgamated zinc, and
amalgamated copper with high hydrogen overpotential as cathodes to electrolytically reduce carbon dioxide in aqueous NaHCO₃ and K₂SO₄ solutions, in which formic acid was the only product.

Most of the reduction reaction of CO₂ occurs in the potential range in which hydrogen evolution reaction (HER) due to hydrolysis of water occurs [4], as the overall standard redox potentials for ERC are in the same range as that for the reduction of protons to H₂. For example [5,6],

\[ E^0, \text{V (SHE)}@298 \text{K (pH} = 14) \]

Cathode: \[ \text{CO}_2(\text{aq} \rightarrow \text{H}_2\text{O} + 2e^- \rightarrow \text{HCOO}^- + \text{OH}^- \] \[ -1.02 \quad (3.1) \]

\[ 2\text{H}_2\text{O} + 2e^- \rightarrow \text{H}_2 + 2\text{OH}^- \] \[ -0.83 \quad (3.2) \]

Reaction (3.1) is considered a kinetically “slow” process, occurring at cathode potentials from about −0.8 to −1.8 V vs. a standard hydrogen electrode (SHE) depending on the CO₂ pressure, current density, and catholyte pH, with overpotential ranging from about −0.4 to −1.4 V. The intrinsic kinetics of Reaction (3.1) is said to be independent of pH (2 < pH < 8), but a pH above 6 can have a strong effect on the mass transfer limiting current for this reaction, as CO₂(aq) is depleted through the CO₂(aq)/HCO₃⁻/CO₃²⁻ equilibria. Reaction (3.2) is thermodynamically favored over Reaction (3.1) over almost the entire pH range at 298 K. However, Reaction (3.1) is kinetically favored over Reaction (3.2) on a group of “high hydrogen overpotential” cathodes, which leads to the high selectivity of formate/formic acid observed by many researchers. The most studied of this favored group of cathode materials are Hg, In, Pb, and Sn, but it is not clear which of these metals is the best because their performance seems to depend on other variables such as CO₂ pressure, catholyte composition, potential, and temperature.

As discussed, increase in the reduction rate of carbon dioxide may also lead to the reduction of water, which will result in hydrogen formation, lowering current efficiency (CE) in ERC. To compete with alternative processes successfully, carbon dioxide reduction must take place at low potential with high efficiency and selectivity at high current densities. The key to this process is to find a stable catalyst with high overpotential for hydrogen evolution and affinity for CO₂, allowing further H⁺ transfer steps selectively toward forming methanol. Alternative ways of suppressing HER include operating at high CO₂ pressure and to use solid polymer electrolyte membrane reactor to increase the availability of CO₂ at the electrocatalyst. Copper, both metallic and in oxides form, is considered a promising electrode material as it offers intermediate hydrogen overvoltage and produces more reduced form of carbon dioxide, such as methanol, ethane, methane, and ethylene. As the potential becomes more negative, the generated carbon monoxide/formate suppresses hydrogen evolution.

Many efforts have been made to fundamental studies of the mechanisms and kinetics of ERC on a variety of electrode surfaces [5,7–9]. The reaction pathways and resulting product distributions can be very complex, because they are not only related to the energies of adsorption of a whole range of possible species, including...
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reactants, intermediates, and products, but also depend on the electrocatalyst property, proton availability, identity of electrolyte and applied cathode potential, carbon dioxide concentration, mass transport, pH, and temperature.

The lowest unoccupied molecular orbital (LUMO) of CO₂ is found predominantly on the carbon atom and most of proposed electrocatalytic reduction mechanisms proceed via high-energy intermediate of \( \cdot \text{CO}_2 \) as shown in Figure 3.1 [10]. The transition between CO₂(ads) and \( \cdot \text{CO}_2 \)(ads) has been suggested to be a common critical limiting step seen by the elbow in plots of \( j \) against overpotential common to most systems regardless of the end product produced [11]. This high-energy intermediate is associated with the changing geometry of the linear CO₂ molecule to the bent \( \cdot \text{CO}_2 \) radical ion, resulting in the observed high overpotential for CO₂ reduction [12]. The detailed mechanistic pathways for each product are not clear at present, and in many cases several different schemes have been proposed. For example, Figure 3.1 shows the most commonly proposed pathways for ERC at Cu electrode in aqueous solution to carbon monoxide, formic acid, methane, ethylene, and ethane [10,11,13–15].

Step A, the adsorption of CO₂ onto the electrode surface was suggested [8,16,17] prior to CO₂ reduction. Sometimes, an intermediate hydration step (step A') is required before the adsorption (step A₂) occurs. In this case, the low solubility of CO₂ in water, that is, 0.070 M at STP conditions, will limit the availability of CO₂(aq) and thus limit the CO₂(ad) concentration on the cathode surface, especially when CO₂ reacts competitively to give HCOO⁻ / CO₃⁻ in alkaline solution. The use of gas phase flow should overcome this limitation by allowing the formation of CO₂(ad) directly from the gaseous state (step A) [11], and catalysts that have high affinity to CO₂ or low activation energy for adsorbing CO₂ should help raise the concentration of CO₂(ad). In addition, ways of increasing CO₂ solubility can be useful in aqueous

![Figure 3.1](https://example.com/f31.png)

**FIGURE 3.1** Mechanistic pathways commonly proposed for ERC at Cu electrode. (Reproduced from the *Electrochimica Acta*, 10, Kaneco, S. et al. Electrochemical reduction of carbon dioxide to ethylene with high Faradaic efficiency at a Cu electrode in CsOH/methanol, 4701–4706, Copyright 1999, with permission from Elsevier.)
systems, such as operating under high pressure or low temperature and using additives to enhance the solubility of CO₂.

Step B is the one-electron reduction of CO₂(ads) to the intermediate radical -CO₂⁻ species, whose standard redox potential is about −1.9 V [18,19] or −1.85 V [20] vs. SHE in aqueous media, −2.21 V vs. saturated calomel electrode (SCE) in dimethylformamide (DMF) [21].

Adsorbed -COOH species formed by the protonation reaction in carboxylic form, unless stabilized, will tend to revert back to M−H+CO₂ or undergo nucleophilic attack to give M−CO⁺ (i.e., M−C=O). This reactive intermediate is thought to be commonly formed for Cu, Ru, and some other d-block metals and is believed to be present in the pathways resulting in highly reduced products.

Step E is the second electronation/protonation to produce a key intermediate species of adsorbed CO for the formation of an adsorbed reactive methylene group, which could be stabilized as CH₄, be dimerized to C₂H₄ or be transformed to C₂H₆.

Pacansky et al. studied self-consistent field (SCF) ab initio molecular orbital energies and atomic population analysis of -CO₂ at the minimum energy geometry (Figure 3.2). According to their analysis, the unpaired electron density at the highest occupied orbital is localized at C atom at 84% [22]. This result suggests that -CO₂ is ready to react as a nucleophilic reactant at the carbon atom. Along this line, the weakly adsorbed -CO₂ goes through a protonation reaction, then there is a second electron transfer to yield formate (steps B–C–D). A parallel disproportionation of the adsorbed -CO₂ radical anion produces CO (steps B–K) [11,14,23].

It is seen from Table 3.1 that the overall standard redox potentials for ERC are in the same range as that for the reduction of protons to H₂ (E⁰ = 0.0 V [SHE]), which indicates that ERC is not thermodynamically much more difficult than hydrogen evolution. However, ERC is kinetically suppressed because of the high-energy intermediate radical -CO₂ and the involvement of multielectron transfer, that is, 2 electrons for HCOO⁻ (steps B–C–D) and 8 electrons for CH₄ (steps B–E–F–G).

Research on ERC is still at a stage of fundamental investigations on mechanisms and kinetics using tiny electrodes (e.g., 1 × 10⁻⁴ m²) with little consideration of the possibility for practical application. Research on the engineering aspects of ERC should be initiated to bridge the gap between the previous laboratory work and industrial reality. Such engineering research includes the design and scale-up of continuous electrochemical reactors, together with the conception, design, and economic projections for complete ERC processes. Akahori et al., who are apparently the first to report continuous operation, used a lead wire bundle cathode in a flow-by reactor with a cation membrane separator. This reactor obtained a formate CE near 100%.

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with single-phase flow of a CO₂-saturated catholyte solution at 1.4 mL min⁻¹ and current about 2 mA (0.02 kA m⁻²). Li and Oloman [24] described the electroreduction of CO₂ in a laboratory bench-scale continuous reactor using a flow-by three-dimensional (3D) cathode of 30# mesh tinned copper, with the variables: current (1–8 A), gas phase CO₂ concentration (16–100 vol%), and operating time (10–180 min), in operation near ambient conditions (ca. 115 kPa [abs], 300 K). For superficial current densities ranging from 0.22 to 1.78 kA m⁻², the measured CE, which is one of the performance indicators for electrochemical processes, for HCOO⁻ = 86%–13%, reactor voltage = 3–6 V, specific energy for HCOO⁻ = 300–1300 kWh kmol⁻¹, space-time yield of HCOO⁻ = 2 × 10⁻⁴–6 × 10⁻⁴ kmol m⁻³ s⁻¹, conversion of CO₂ = 20%–80%, and yield of organic products from CO₂ = 6%–17%. The initial electroactive species in a primary reaction is subjected to CO₂ mass transfer constraint, with CE depending on the current density and partial pressure of CO₂ in the gas phase, together with the hydrogen overpotential and mass transfer capacity of the 3D cathode. Figure 3.3 shows the process flow diagram.

### 3.2 ELECTROCHEMICAL KINETICS

#### 3.2.1 Certain Aspects of Electrochemical Kinetics

The electrochemical reaction occurs at the interface between the electrode (an electronic conductor) and electrolyte solution (an ionic conductor), composed of a series of steps always includes these three steps: (1) the approach of the reactant species to the electrode surface (first mass transfer); (2) the reaction via heterogeneous electron

<table>
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<th>E⁰/V vs. SHEb</th>
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<tr>
<td>CO₂ + e⁻ = · CO₂⁻</td>
<td>-1.90</td>
<td>-</td>
</tr>
<tr>
<td>CO₂ + 2H⁺ + 2e⁻ = CO + H₂O</td>
<td>-0.10</td>
<td>-0.52</td>
</tr>
<tr>
<td>CO₂ + 2H⁺ + 2e⁻ = HCOOH</td>
<td>-0.20</td>
<td>-0.61</td>
</tr>
<tr>
<td>2CO₂ + 2H⁺ + 2e⁻ = H₂C₂O₄</td>
<td>-0.475</td>
<td>-0.889</td>
</tr>
<tr>
<td>CO₂ + 4H⁺ + 4e⁻ = HCHO + H₂O</td>
<td>-0.071</td>
<td>-0.485</td>
</tr>
<tr>
<td>CO₂ + 6H⁺ + 6e⁻ = CH₃OH + H₂O</td>
<td>0.03</td>
<td>-0.38</td>
</tr>
<tr>
<td>CO₂ + 8H⁺ + 8e⁻ = CH₄ + 2H₂O</td>
<td>0.17</td>
<td>-0.24</td>
</tr>
<tr>
<td>2CO₂ + 12H⁺ + 12e⁻ = C₂H₄ + 4H₂O</td>
<td>0.07</td>
<td>-0.34</td>
</tr>
<tr>
<td>2CO₂ + 12H⁺ + 12e⁻ = C₂H₅OH + 3H₂O</td>
<td>0.085</td>
<td>-0.3287</td>
</tr>
<tr>
<td>3CO₂ + 18H⁺ + 18e⁻ = C₃H₇OH + 5H₂O</td>
<td>0.09</td>
<td>-0.3237</td>
</tr>
<tr>
<td>2H⁺ + 2e⁻ = H₂</td>
<td>0</td>
<td>-0.414</td>
</tr>
</tbody>
</table>

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Transfer across the interface (actual electrochemical step); and (3) the movement of the product species away from the reaction area into bulk solution (second mass transfer). The actual electrochemical step can be accompanied by different chemical reactions, either in bulk or on the electrode surface. Some of these processes, such as electron transfer at the electrode surface or adsorption, depend upon the electrode potential. Determination of a possible step order and the rate-determining step (r.d.s.) is crucial for the dynamic description of a specific electrode process [25].

For a given electrode reaction:

\[
O + n\text{e}^- \overset{k_f}{\longrightarrow} R
\]

where both oxidized form, O, and reduced form, R, of a redox couple are initially present in the bulk solution.

The rate of the forward reduction process, \( v_f \), is

\[
v_f = k_f C_O(0,t) = \frac{i_c}{nFA}
\]

whereas the rate of the backward oxidation reaction, \( v_b \), is

\[
v_b = k_b C_R(0,t) = \frac{i_a}{nFA}
\]

where \( k_f/k_b \) is the forward/backward rate constant, \( C_O(0,t)/C_R(0,t) \) is the surface concentration of O/R at time \( t \), and \( i_c/i_a \) is the cathodic/anodic current. The net reaction rate is

\[
v_{net} = v_f - v_b = k_f C_O(0,t) - k_b C_R(0,t) = \frac{i}{nFA}
\]
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In which the overall current is

$$i = i_c - i_a = nF[A_kC_O(0,t) - k_bC_R(0,t)]$$  \hspace{1cm} (3.7)

An accurate kinetic picture of an electrode process is often gained by determining current as a function of potential because there is a proportionality between the current and the net rate of an electrode reaction, and the reaction rate is a strong function of the electrode potential. At equilibrium, the net current is zero, and the electrode potential is defined by the Nernst equation:

$$E = E^{0'} + \frac{RT}{nF} \ln \frac{C^*_O}{C^*_R}$$  \hspace{1cm} (3.8)

where $C^*_O/C^*_R$ is the bulk concentration of O/R, and $E^{0'}$ is the former potential. Upon passage of Faradaic current, the electrode potential deviates from its equilibrium value and this is termed electrode polarization. The extent of polarization is determined by the overpotential, $\eta$.

$$\eta = E - E_{eq}$$  \hspace{1cm} (3.9)

Based on Butler–Volmer’s model of electrode kinetics, for a single one-step, one-electron reversible electrode process without any other chemical step

$$O + e \rightleftharpoons R$$  \hspace{1cm} (3.10)

The derived current–overpotential equation is

$$i = i_0 \left[ \frac{C_O(0,t)}{C^*_O} e^{-\alpha \eta} - \frac{C_R(0,t)}{C^*_R} e^{(1-\alpha) \eta} \right]$$  \hspace{1cm} (3.11)

where $f = F/RT$, $\alpha$ is the transfer coefficient, and $i_0$ is the exchange current, which represents the balanced Faradaic current at equilibrium and is equal to either component current, $i_c$ or $i_a$ in magnitude. The value of $i_0$ can be calculated by

$$i_0 = FAk^0C^*_Oe^{-af(E_{eq} - E^{0'})}$$  \hspace{1cm} (3.12)

The curve in Figure 3.4 shows the behavior of Equation 3.11, from which we can see that for the cathodic branch at high $\eta$, the anodic component $i_a$ is insignificant, whereas the anodic contribution $i_c$ is negligible at large positive overpotentials, and the total current is the sum of the components $i_c$ and $i_a$. At extreme $\eta$, the current levels off, reaching a cathodic limiting current, $i_{l,c}$ or an anodic limiting current, $i_{l,a}$.
which is limited by mass transfer rather than heterogeneous kinetics and the overpotential is a concentration overpotential. At certain $\eta$, the electrode process could have several slow steps and the current is driven by overpotentials associated with different reaction steps: $\eta_{\text{mt}}$ (mass transfer overpotential), $\eta_{\text{ct}}$ (charge-transfer overpotential), and $\eta_{\text{r} \times n}$ (the overpotential associated with a preceding reaction).

The actual relationship between the current and the electrode overpotential usually depends on the nature of the limiting step, which allows hypothesizing about the character of the investigated process.

1. No mass transfer effects

When mass transfer effects are not included, Equation 3.11 becomes

$$i = i_0[\nu^{\alpha/\eta} - \nu^{(1-\alpha)/\eta} - e^{\nu_{\text{eq}}}] \frac{\nu}{i_0}$$

(3.13)

known as the Butler–Volmer equation historically. The overpotential here is solely for driving the heterogeneous process at the rate reflected by the current. The lower the exchange current, the larger the activation overpotential for any particular net current, indicating more sluggish kinetics.

2. Linear characteristic at small $\eta$

When the value of $\eta$ is sufficiently small, Equation 3.11 can be expressed as

$$i = -i_0 f \eta$$

(3.14)
which indicates that the corresponding $i - \eta$ curve near $E_{eq}$ in a narrow potential range is linear with negative reciprocal slope of $-\eta/i$, which is often called the charge-transfer resistance, $R_{ct}$

$$R_{ct} = \frac{RT}{Fi_0}$$ (3.15)

serving as a convenient index of kinetic facility.

3. Tafel behavior at large $\eta$

At large negative/positive overpotentials, one of the bracketed terms in Equation 3.13 becomes negligible. When $\exp(-\alpha \eta) \gg \exp((l - \alpha)\eta)$ for a cathodic branch, Equation 3.13 becomes

$$i = i_0 e^{-\alpha \eta}$$ (3.16)

or expressed as

$$\eta = \frac{RT}{\alpha F} \ln i_0 - \frac{RT}{\alpha F} \ln i$$ (3.17)

Compared with the empirical Tafel equation given by Tafel in 1905

$$\eta = a + b \log i$$ (3.18)

the constants can now be identified from theory as [25]

$$a = \frac{2.3RT}{\alpha F} \log i_0, \quad b = -\frac{2.3RT}{\alpha F}$$ (3.19)

Tafel behavior is an indicator of totally irreversible kinetics. A plot of $\log i$ vs. $\eta$, known as a Tafel plot (Figure 3.6), is useful for the evaluation of kinetic parameters, such as $\alpha$, $i_0$ when applied, though it sharply deviates from linear behavior when $\eta$ approaches zero.

### 3.2.2 Overpotentials

#### 3.2.2.1 Basic Concept

The overpotential is the difference between the applied electrode potential, $E_{applied}$, and $E^0$ (products/substrates), at a given current density, reflecting the degree of deviation of the electrode potential from its thermodynamic equilibrium value from the Nernst equation. In other words, an overpotential is the extra amount of nonreversible energy required to overcome the energy barrier which allows the reaction to occur. It shows how far away the electrode is from its equilibrium.
The electrode overpotential mainly consists of three components: concentration overpotential, $\eta_{\text{con}}$; activation overpotential, $\eta_{\text{act}}$; and ohmic overpotential, $\eta_{\text{ohmic}}$, expressed as follows:

$$\eta = \eta_{\text{ohmic}} + \eta_{\text{con}} + \eta_{\text{act}}$$

(3.20)

where $\eta$ is the overall overpotential. Other additional overpotentials may exist, such as the chemical reaction overpotential. The cell overpotential cannot be eliminated but can be minimized by proper material modification and good cell design. Furthermore, cell working atmosphere, such as pressure and temperature, can also influence the overpotential.

### 3.2.2.1.1 Ohmic Losses

The ohmic losses are due to resistance created when ions are moving through the electrolyte and electrons moving through the electrode, including the Pt lead wire resistance, electrode resistance, electrolyte resistance, etc. According to Ohm’s law:

$$\eta_{\text{ohmic}} = IR$$

(3.21)

where $R$ is the ohmic resistance. By knowing the conductivity ($\kappa$), conducting length ($l$), and cross-section area ($A_0$), the ohmic resistance of such geometry can be calculated by

$$R = \frac{l}{\kappa A_0}$$

(3.22)

Equipotential plane is required to estimate the ohmic resistance of a conductor when the above equation is used. The resistance of a lead wire can be easily evaluated by knowing its conductivity. However, the electrolyte and electrode resistances cannot be directly estimated because the electrochemical reactions at the interface of the electrode and electrolyte cause a nonequipotential plane. An average ohmic resistance is sought. For example, a porous Pt electrode can be viewed as numerous cylindrical pores surrounded by Pt blocks. Each Pt block and electrolyte forms a resistor, as illustrated in Figure 3.5.

The average resistance can therefore be calculated as these numerous resistors are aligned in parallel:

$$R = \frac{l}{\kappa(1-\varepsilon)A_0}$$

(3.23)

where $\varepsilon$ is the electrode porosity, and $A_0$ is the electrode physical area. Equation 3.23 is based on assuming the potential field of each single resistor does not interfere with each other. From the above equations, the electrode and electrolyte resistances can be estimated and compared with experimental measurement.
3.2.2.1.2 Concentration Overpotential

A concentration overpotential is caused by the slow diffusion of reactants or products under concentration gradients. It is defined as an external energy required to maintain concentration gradients near the electrode for the sustenance of chemical reactions. This concentration overpotential becomes eminent as mass diffusion effects hinder the entire electrode reaction. For CO₂ electroreduction, mass diffusion includes gas bulk diffusion and adsorbates surface diffusion. When the maximum diffusion rate of transporting species to/from the electrode reaction site is slower than the electrochemical reaction rate, diffusion becomes a rate-determining step, and a limiting current is reached.

By Fick’s diffusion law [27], the limiting current density can be calculated by assuming the reactant concentration at the reaction site is zero:

\[
i_L = \frac{nFD\zeta}{\delta}
\]

(3.24)

where \(D\) is the diffusivity, \(C_\zeta\) is the reactant bulk concentration, and \(\delta\) is the thickness of the diffusion layer. Assuming the charge-transfer reaction rate at the electrode is so high that the activation overpotential is negligible compared with the concentration overpotential. The concentration overpotential can therefore be written as

\[
\eta_{\text{con}} = \frac{RT}{nF} \ln \left(1 - \frac{i}{i_L}\right)
\]

(3.25)

The concentration overpotential can be reduced by increasing the limiting current, which is a function of concentration and diffusivity as expressed in Equation 3.24. Design of gas bulk diffusion channels and microstructures of an electrode can influence the concentration overpotential.

3.2.2.1.3 Activation Overpotential

Activation overpotential describes an external energy required to overcome the maximum activation energy barrier in order to maintain the electrode reaction at an
appreciable rate. This irreversible potential occurs when the rate of the electrochemical reaction at the electrode is limited by slow electrode kinetics, or charge transfer. It highly depends on the electrode catalytic characteristics.

Activation overpotentials are affected mostly by the oxidation or reduction rate constants. A decrease in the oxidation or reduction rate constant will increase the activation overpotential. The magnitude of the activation overpotential is more than doubled as the redox rate constant decreases by a magnitude of order two. Therefore, one efficient way to improve the CO₂ electroreduction performance is to find a better catalyst with a fast oxidation/reduction rate constant to reduce the activation overpotential. Both the anode and cathode activation overpotentials follow the Tafel behavior, and the charge transfer controls the reaction as discussed below.

### 3.2.2.2 Butler–Volmer Equation

As discussed in Section 3.2.1, for an electrochemical reaction with multiple steps involving one electron without any other chemical step, the activation overpotential can be correlated to current by the Butler–Volmer equation (3.13).

The transfer coefficients are considered as the fraction of the change in polarization, which leads to a change in the reaction rate constant. The transfer coefficients can be given by the Bockris model as [28]

\[ \alpha_a = \frac{n - \gamma_c}{\upsilon} - r\beta \]  \hspace{1cm} (3.26)

\[ \alpha_c = \frac{\gamma_c}{\upsilon} + r\beta \]  \hspace{1cm} (3.27)

where \( \alpha_a \) and \( \alpha_c \) are the anodic and cathodic transfer coefficients, respectively. \( \gamma_c \) is the number of charges transferred ahead of the r.d.s., \( \upsilon \) is the total number of times of repeating the r.d.s. reaction to complete the reaction, \( r \) is the number of charges transferred in the r.d.s., and \( \beta \) is the symmetric coefficient (usually 0.5). Apparently, the transfer coefficients have the following relationship:

\[ \alpha_a + \alpha_c = \frac{n}{\upsilon} \]  \hspace{1cm} (3.28)

The exchange current density is a function of reaction rate constants, the concentration of the anodic and cathodic reactants, etc. It is related to the balanced forward and backward electrode reaction rates at equilibrium. A high exchange current density leads to a fast electrochemical reaction, thus good cell performance is anticipated.

A typical Butler–Volmer equation at large activation overpotential is plotted in Figure 3.6 when the exchange current density is 0.001 mA/cm² and the anodic and cathodic transfer coefficients are unity. The plot shows a high linearity, indicating the Tafel behavior. The plot is symmetric due to the same anodic and cathodic transfer coefficients. Otherwise, it should be asymmetric.
Electrode Kinetics of CO$_2$ Electroreduction

3.2.2.3 Overpotential of CO$_2$ Electroreduction

Direct ERC on most electrode surfaces requires impractically high overpotential which is necessary to drive the process and consequently lowers the conversion efficiency [29].

The standard potential of the reduction of CO$_2$ to different products as shown in Table 3.1, calculated from the thermodynamic data, is much more positive than that the reduction actually takes place at as shown in Table 3.2. Such high overpotential is presumed from involvement of intermediate species, $\cdot CO_2$ anion radical, which requires highly negative potential for the formation. The high overpotential depends on electrode metal, crystal orientation, and reduction product alongside proton availability. CO formation takes place with relatively lower overpotentials than HCOO$^-$ formation. Stabilization of $\cdot CO_2$ adsorption on electrodes may lead to decrease of overpotential [30]. Coordination of the CO$_2$ to M can activate $\cdot CO_2$ and promote its reductive disproportionation to form CO + CO$_3^{2-}$.

Clearly, in order to minimize overpotentials, catalysts need to be developed that have formal potentials $E^{0}(\text{Cat}^{n+0})$ well matched to $E^{0}(\text{products/CO}_2)$, and appreciable rate constants for the electroreduction of CO$_2$ to appropriate products at this potential. In addition, the heterogeneous rate constant for reduction of the electrocatalyst at the electrode must be high for $V_{\text{applied}}$ near $E^{0}(\text{Cat}^{n+0})$.

Transition metal electrodes have been reported to dramatically reduce the overpotential of reduction to at least 500 mV anodic of $E^0$ for CO$_2$ $\rightarrow$ CO$_2$. Bruce et al. [32] find $E^0 = +0.1$ V vs. SHE for CO$_2$ + 2H$^+$ + 2e$^- \rightarrow$ HCOOH on copper, which is much more positive than that calculated from Gibbs energy of formation.
### TABLE 3.2

Potential and Faradaic Efficiencies of Products of CO\(_2\) Reduction at Various Metal Electrodes in 0.1 M KHCO\(_3\), 
\(T = 18.5 \pm 0.5^\circ\mathrm{C}\)

<table>
<thead>
<tr>
<th>Electrode</th>
<th>Potential vs. SHE V</th>
<th>Current Density (mA cm(^{-2}))</th>
<th>Faradaic Efficiency (%)</th>
</tr>
</thead>
<tbody>
<tr>
<td>Pb</td>
<td>−1.63</td>
<td>5.0</td>
<td>CH(_4) C(_2)H(_4) EtOH(^b) PrOH(^b) CO HCOO(^{-}) H(_2) Total</td>
</tr>
<tr>
<td>Hg</td>
<td>−1.51</td>
<td>0.5</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 99.5 0.0 99.5</td>
</tr>
<tr>
<td>Tl</td>
<td>−1.60</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 21.4 94.9 3.3 100.3</td>
</tr>
<tr>
<td>In</td>
<td>−1.55</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 7.1 88.4 4.6 100.1</td>
</tr>
<tr>
<td>Sn</td>
<td>−1.48</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 7.1 88.4 4.6 100.1</td>
</tr>
<tr>
<td>Cd</td>
<td>−1.63</td>
<td>5.0</td>
<td>1.3 0.0 0.0 0.0 0.0 0.0 0.0 13.9 78.4 9.4 103.0</td>
</tr>
<tr>
<td>Au</td>
<td>−1.14</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 87.1 0.7 10.2 98.0</td>
</tr>
<tr>
<td>Ag</td>
<td>−1.37</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 81.5 0.8 12.4 94.6</td>
</tr>
<tr>
<td>Zn</td>
<td>−1.54</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 79.4 6.1 9.9 95.4</td>
</tr>
<tr>
<td>Pd</td>
<td>−1.20</td>
<td>5.0</td>
<td>2.9 0.0 0.0 0.0 0.0 0.0 0.0 28.3 2.8 26.2 60.2</td>
</tr>
<tr>
<td>Ga</td>
<td>−1.24</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 23.2 0.0 79.0 102.0</td>
</tr>
<tr>
<td>Cu</td>
<td>−1.44</td>
<td>5.0</td>
<td>33.3 25.5 5.7 3.0 0.0 0.0 0.0 1.3 94.4 20.5 103.5(^c)</td>
</tr>
<tr>
<td>Ni</td>
<td>−1.48</td>
<td>5.0</td>
<td>1.8 0.1 0.0 0.0 0.0 0.0 0.0 1.4 88.9 92.4(^d)</td>
</tr>
<tr>
<td>Fe</td>
<td>−0.91</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 94.8 94.8</td>
</tr>
<tr>
<td>Pt</td>
<td>−1.07</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0.1 95.7 95.8</td>
</tr>
<tr>
<td>Ti</td>
<td>−1.60</td>
<td>5.0</td>
<td>0.0 0.0 0.0 0.0 0.0 0.0 0.0 not available 0.0 99.7 99.7</td>
</tr>
</tbody>
</table>


\(^{a}\) Ethanol.  
\(^{b}\) \(n\)-propanol.  
\(^{c}\) The total value contains C\(_3\)H\(_7\)OH (1.4%), CH\(_3\)CHO (1.1%), and C\(_2\)H\(_5\)CHO (2.3%) in addition to the tabulated substances.  
\(^{d}\) The total value contains C\(_2\)H\(_6\) (0.2%).
Fundamental studies will contribute to enhancement of our understanding of the overpotential of the electrodes. A wide range of Tafel slopes for CO$_2$ reduction from 120 mV decade$^{-1}$ to 350 mV decade$^{-1}$ has been reported [5,16,33,34]. These slopes indicate a rate-determining initial electron transfer to CO$_2$ forming a surface adsorbed $\cdot$CO$_2$ intermediate. The calculated exchange current density for the formation of $\cdot$CO$_2$ radical at 100 kPa and 298 K in CO$_2$-saturated aqueous solution (~0.036 M) is $4.8 \times 10^{-7}$ kA m$^{-2}$ [35]. The exchange current densities for ERC to formate at 293 K in 0.95 M KCl$^+$0.05 M NaHCO$_3$ on In, Hg, and Sn are reported, respectively, as $1 \times 10^{-7}$, $1 \times 10^{-10}$, $1 \times 10^{-8}$ kA m$^{-2}$ [6].

Gold electrodes yield CO in CO$_2$ reduction at $-0.8$ V vs. SHE with a low overpotential in 0.5 M KHCO$_3$ [30]. The obtained relationship between the potential and logarithm of the partial current of CO formation ($i_c$) (Figure 3.7) showed that the Tafel slope is approximately 130 mV decade$^{-1}$ in the lower current region, where the transport process of CO$_2$ does not interfere with the supply of CO$_2$ to the electrode, the Tafel slope corresponds to the transfer coefficient 0.46. $i_c$ at a constant potential is linear to the CO$_2$ partial pressure. These data suggest that the CO$_2$ reduction proceeds in the first order with respect to CO$_2$, and the r.d.s. of the reaction is the first electron transfer to CO$_2$. These facts support the reaction scheme discussed in the
Electrochemical Reduction of Carbon Dioxide

Following. In phosphate buffer solutions of pH 2–6.8 at an Au electrode, \( i_c \) is proportional to the pressure of \( \text{CO}_2 \) [36]. The Tafel slope is ca. 120 mV decade\(^{-1}\). The potential partial current relation obtained with electrolytes at pH below 4.3 agreed well with that obtained with 0.5 M KHCO\(_3\) at pH 7.5 after the double-layer correction due to the difference of the electrolyte concentration [30]. This fact shows that CO formation at Au electrode does not depend on pH of the electrolyte, and that the proton donor is not \( \text{H}^+ \) but \( \text{H}_2\text{O} \) molecules.

The intrinsic electrocatalytical activity of nanoporous silver (np-Ag) for \( \text{CO}_2 \) reduction to CO was investigated through Tafel analysis in a \( \text{CO}_2 \)-saturated 0.5 M KHCO\(_3\), compared with polycrystalline Ag catalyst, as shown in Figure 3.8 [37]. As observed, the np-Ag was more preferred for \( \text{CO}_2 \) reduction with a Tafel slope of 58 mV decade\(^{-1}\), much smaller than that of 132 mV decade\(^{-1}\) for polycrystalline Ag. At a overpotential higher than 0.25 V, the slope increased sharply, indicating another rate-limiting step most probably relating to the issues of the diffusion of reactants and products out of/into the catalyst nanopores. Mechanistically, there are two steps in the two-electron reduction of \( \text{CO}_2 \) to CO on an Ag surface [38]. First, one electron is transferred to a \( \text{CO}_2 \) molecule, forming a \( \cdot\text{CO}_2^- \) anion intermediate absorbed on the catalyst surface. Subsequently, the \( \cdot\text{CO}_2^- \) anion takes another electron and two protons, forming a molecule of CO and a molecule of \( \text{H}_2\text{O} \). As reported [39], the first step at a much more negative potential compared with that of the following step is rate determining for the whole process with calculated Tafel slope of 120 mV decade\(^{-1}\). This is very similar to that of 132 mV decade\(^{-1}\) observed in polycrystalline Ag. For np-Ag, the sharp decrease of Tafel slope at 58 mV decade\(^{-1}\) presents a fast step of initial electron transfer before a r.d.s. of later nonelectron transfer [39–41], indicating that the np-Ag with possibly higher index facets supported by

![Figure 3.8](image-url)
the highly curved surface [42,43] are able to stabilize the anion \( -\text{CO}_2 \) intermediate much better than a flat one.

Results of studies on the kinetics with a copper foil electrode at 273 and 295 K using two separate electrode pretreatments to remove the oxide layer, that is, 10 wt% HCl and 10 wt% HNO\(_3\) [44], is listed in Table 3.3.

The kinetic information/data on ERC is sparse and difficult to summarize because of the variety of approaches and experimental conditions. It has to be noted that the reaction kinetics depend on many interacting factors so results obtained by one researcher under his conditions might not apply under other conditions.

### 3.3 MASS TRANSFER NEAR THE ELECTRODE SURFACE

#### 3.3.1 Fick’s Laws

Diffusion is one of the fundamental processes by which material moves, the macroscopic result of random molecular motion describing the spread of particles, and is an important factor controlling the rate at which many interactions occur. The diffusion coefficient \( (D) \) is a parameter indicative of the diffusional mobility of species and encountered most famously in Fick’s laws (3.29) and (3.30), but also in numerous other equations throughout physics and chemistry. Fick’s first law of diffusion states [45]

\[
J = -D \frac{\partial C(x)}{\partial x} \tag{3.29}
\]

where \( J \) is the diffusion flux, \( D \) is the diffusion coefficient, \( C \) is concentration, and \( x \) is the position in the one-dimensional system. This proportionality of flux of matter to the concentration gradient (3.29) shows that the flux of matter is dependent upon the variation in concentration with position. From this relationship, it is suggested that without a concentration gradient there is no net flux and the diffusive flux would

---

**TABLE 3.3**

Kinetic Information of CO\(_2\) Electroreduction to CH\(_4\) on a Cu Foil Cathode

<table>
<thead>
<tr>
<th>Temperature (K)</th>
<th>Pretreatment</th>
<th>Tafle Slope V/decade</th>
<th>( j_o ) kA m(^{-2} )</th>
<th>Highest CE %</th>
<th>CE at (-1.46 \text{ V (SHE)}) %</th>
</tr>
</thead>
<tbody>
<tr>
<td>273</td>
<td>10 wt% HCl</td>
<td>0.539</td>
<td>N/A</td>
<td>N/A</td>
<td>47</td>
</tr>
<tr>
<td>295</td>
<td>10 wt% HCl</td>
<td>0.110</td>
<td>1.94 \times 10(^{-7})</td>
<td>50</td>
<td>20</td>
</tr>
<tr>
<td>295</td>
<td>10 wt% HNO(_3)</td>
<td>0.170</td>
<td>N/A</td>
<td>32</td>
<td>N/A</td>
</tr>
</tbody>
</table>

*Source:* Reproduced from *Journal of Electroanalytical Chemistry and Interfacial Electrochemistry*, 245(1–2), Kim, J. J. et al. Reduction of CO\(_2\) and CO to methane on Cu foil electrodes, 223–244, Copyright 1988, with permission from Elsevier.

*Note:* Catholyte = 0.5 M KHCO\(_3\) at pH = 7.6.
be zero. This first law describes mathematically diffusion within steady-state systems where the concentration is time invariant; however, this is not always the case, which leads to the less specific second law. Fick’s second law of diffusion [45]

\[
\frac{\partial C(x,t)}{\partial t} = - \frac{\partial J}{\partial x} = D \frac{\partial^2 C}{\partial x^2}
\]  

(3.30)

Fick’s second law of diffusion (3.30) predicts the change in concentration (accumulation or depletion) with time as a result of diffusion with \( t \) denoting the time. The concentration change is proportional to the diffusion coefficient and the second derivative/curvature of the concentration as illustrated in Figure 3.9. This equation assumes that the diffusion coefficient is independent of composition or the range of compositions is small.

The diffusion coefficient of a species in a given system can be evaluated using the Stokes–Einstein (3.31) and Wilke–Chang (3.32) relations [47,48]:

\[
D = \frac{k_B T}{6\pi\eta r}
\]

(3.31)

\[
D = \frac{7.4 \times 10^{-8}(xM)^{1/2}T}{\eta V^{0.6}}
\]

(3.32)

In the Stokes–Einstein equation (3.31), \( k_B \) is the Boltzmann constant, \( T \) is the temperature in K, \( \eta \) is the dynamic viscosity in Pa·s, and \( r \) is the molecular radius of the analyte in m to give \( D \) in m² s⁻¹. In the Wilke–Chang relationship (3.32), \( x \) is the association parameter of the solvent, \( M \) is the molecular mass of the solvent in u, \( T \) is the temperature in K, \( \eta \) is the dynamic viscosity in cP or mPa·s, and \( V \) is the molar volume of analyte at boiling point under standard conditions in cm³ mol⁻¹ to give the diffusion coefficient in cm² s⁻¹. Some of the most well utilized electrochemical
Electrode Kinetics of CO$_2$ Electroreduction

Techniques have diffusion as the primary form of mass transport and as such D is a useful parameter to define and can be measured experimentally.

### 3.3.2 Solubility of CO$_2$

Traditionally, most of the CO$_2$ reduction research has been carried out in aqueous media. The solubility of CO$_2$ in aqueous electrolyte is quite low, which results in poor mass transport of CO$_2$ to the electrode, and is the limitation to obtain high selectivity at high current density. Under moderate experimental conditions, considering CO$_2$ solubility in water is 30 mM at 1 atm at ambient temperature, the highest current density will be restricted to 20 mA cm$^{-2}$ or so for formation of CO or HCOO$^-$, for example. Such a low transport process must be improved by any means, if the CO$_2$ reduction is utilized for a practical process. Various solutions have been proposed, such as overcoming by operating at elevated pressure, decreased temperature, in alternate organic media, or using 3D electrodes, such as gas diffusion electrodes (GDEs), solid polymer electrolytes, and packed-bed electrodes. As reported, the solubility of CO$_2$ in water increases with the decrease in temperature (Table 3.4), for example, 0.058 mol L$^{-1}$ at 269 K compared with 0.033 mol L$^{-1}$ at 298 K under ambient pressure. At 60 atm and 25°C, the solubility of CO$_2$ in water is over 1 mol L$^{-1}$. Solubility is also increased through alteration of the solvent system. In methanol, the solubility of CO$_2$ is over 1 mol L$^{-1}$ at 25°C and 8 atm, a considerably lower pressure than that required to maintain an equivalent concentration in an aqueous system.

The solubility of CO$_2$ is of great importance for developing the process of ERC because it determines the concentration of CO$_2$ in the liquid phase (CO$_2$(aq)), which affects the rate of CO$_2$ mass transfer to the cathode surface and thus the corresponding product CE.

### 3.3.3 Influences of CO$_2$ Mass Transfer Near the Electrode Surface

When CO$_2$ gas is in contact with an aqueous solution, CO$_2$ is absorbed into the liquid phase as loosely hydrated CO$_2$(aq) (Equation 3.33) that subsequently engages in a relatively slow reaction with water to form carbonic acid, H$_2$CO$_3$ [51–54].

\[
\text{CO}_2\text{(g)} \rightleftharpoons \text{CO}_2\text{(aq)}
\]  

(3.33)

<table>
<thead>
<tr>
<th>Table 3.4</th>
</tr>
</thead>
<tbody>
<tr>
<td>Solubility of CO$_2$ in Water (mol/L at 101 kPa CO$_2$ Partial Pressure)</td>
</tr>
<tr>
<td>T, °C</td>
</tr>
<tr>
<td>S</td>
</tr>
</tbody>
</table>
Electrochemical Reduction of Carbon Dioxide

\[
\text{CO}_2(\text{aq}) + \text{H}_2\text{O} \rightleftharpoons \frac{k_{i0}}{k_o} \text{H}_2\text{CO}_3(K^\#) \quad (3.34)
\]

For Equation 3.34, the forward reaction \((k_{i0} = 3.0 \times 10^{-2} \text{ s}^{-1})\) is much slower than the reverse reaction \((k_o = 23.7 \text{ s}^{-1})\) at 298 K. As less than 1% of the dissolved \(\text{CO}_2\) is present as \(\text{H}_2\text{CO}_3\), Reactions (3.33) and (3.34) are combined to give the pseudo-equilibrium:

\[
\text{CO}_2(\text{g}) + \text{H}_2\text{O(l)} \rightleftharpoons \text{H}_2\text{CO}_3^\#(K_0) \quad (3.35)
\]

in which \([\text{HCO}_3^\#] = [\text{CO}_2(\text{aq})] + [\text{H}_2\text{CO}_3]\).

In basic solutions (pH > 7), \(\text{CO}_2(\text{aq})\) may react directly with \(\text{OH}^-\):

\[
\text{CO}_2(\text{aq}) + \text{OH}^- \rightleftharpoons \frac{k_{i1}}{k_{i1}} \text{HCO}_3^- \quad K_1' \quad (3.36)
\]

where the forward reaction \((k_{i1} = 8.5 \times 10^3 \text{ M}^{-1} \text{ s}^{-1})\) is much faster than the reverse reaction \((k_{i1} = 2.3 \times 10^{-4} \text{ s}^{-1})\) at 298 K.

The rate of \(\text{CO}_2\) absorption into the catholyte is determined by the rates of Reactions (3.34) and (3.36) and greatly affected by the physical diffusion rate of \(\text{CO}_2\) (Equation 3.33, mass transfer step) through the boundary layers at the gas/liquid (G/L) interface, which is strongly influenced by the way \(\text{CO}_2\) gas is contacted with the liquid.

Combining Equations 3.33, 3.34, and 3.35 gives the mass transfer step as the following equation shows [55,56]. Equations 3.34 and 3.36 are the two thermochemical reaction paths that consume \(\text{CO}_2(\text{aq})\) [56]:

**Mass transfer step:**

A. \(\text{CO}_2(\text{g}) + \text{H}_2\text{O(l)} \rightleftharpoons \text{CO}_2(\text{aq}) + \text{H}_2\text{O(l)} \equiv \text{H}_2\text{CO}_3^\#\)

**Chemical reactions steps:**

B. \(\text{CO}_2(\text{aq}) + \text{H}_2\text{O} \rightleftharpoons \frac{k_{i0}}{k_o} \text{H}_2\text{CO}_3 \rightleftharpoons \text{H}^+ + \text{HCO}_3^-\)

C. \(\text{CO}_2(\text{aq}) + \text{OH}^- \rightleftharpoons \frac{k_{i1}}{k_{i1}} \text{HCO}_3^-\)

For the mass transfer step A, the rate is given by

\[
MT_{rate} = k_{G/L} a p_{\text{CO}_2} K_0 \quad (3.37)
\]

where:

- \(k_{G/L}\) = the mass transfer coefficient (m s\(^{-1}\))
- \(a\) = the specific G/L surface area (m\(^2\) m\(^{-3}\))
- \(p_{\text{CO}_2}\) = the \(\text{CO}_2\) partial pressure (kPa)
- \(K_0\) = the equilibrium constant for Equation 3.35, that is, \(2.94 \times 10^{-4} \text{ M}^{-1} \text{ s}^{-1} \text{ M kPa}^{-1}\) at 298 K [55].
For the thermochemical reaction steps, for pH < 8, step B dominates and the chemical reaction rate is

\[ -\frac{d[CO_2(aq)]}{dt} = k_{i0}h_L \varepsilon[CO_2(aq)] = 3 \times 10^{-2} h_L \varepsilon[CO_2(aq)] \]  \hspace{1cm} (3.38)

where:
- \( k_{i0} \) = rate constant of reaction 3.34 (s\(^{-1}\))
- \( h_L \) = liquid hold-up (–)
- \( \varepsilon \) = voidage of the 3D cathode (–)
- \([CO_2(aq)]\) = concentration of dissolved CO\(_2\) in the catholyte (M).

At pH > 10, step C is predominant and the rate of CO\(_2\)(aq) consumption is

\[ -\frac{d[CO_2(aq)]}{dt} = k_{i1}h_L \varepsilon[CO_2(aq)][OH^-] = 8.5 \times 10^3 h_L \varepsilon[CO_2(aq)][OH^-] \]  \hspace{1cm} (3.39)

where:
- \( k_{i1} \) = rate constant of reaction 3.36 (s\(^{-1}\)).

In the pH range of 8–10, both steps are important, hence the rate should be

\[ -\frac{d[CO_2(aq)]}{dt} = (3.0 \times 10^{-2} + 8.5 \times 10^3[OH^-])h_L \varepsilon[CO_2(aq)] \]  \hspace{1cm} (3.40)

Table 3.5 shows the calculated mass transfer rate and total thermochemical reaction rates at different pH values where CO\(_2\) partial pressure and temperature are 145 kPa and 298 K, respectively.

Comparing the mass transfer and thermochemical reaction rates, it may be seen that when a catholyte solution of carbonate or of low ratio of bicarbonate/carbonate is fed, that is, pH is higher than about 10, the chemical reaction is so

<table>
<thead>
<tr>
<th>pH</th>
<th>7.5</th>
<th>8.5</th>
<th>9.5</th>
<th>10.5</th>
</tr>
</thead>
<tbody>
<tr>
<td>Mass transfer rate (M s(^{-1}))</td>
<td>0.025</td>
<td></td>
<td></td>
<td></td>
</tr>
<tr>
<td>Chemical reaction rate (M s(^{-1}))</td>
<td>0.0003</td>
<td>0.0006</td>
<td>0.003</td>
<td>0.03</td>
</tr>
</tbody>
</table>

Table 3.5 Estimated Mass Transfer and Thermo-Chemical Reaction Rates at Different pH.
fast that one cannot expect to have both a relatively high concentration of CO$_2$(aq) and high bulk pH simultaneously. Hence, depending on the CO$_2$ pressure, G/L mass transfer capacity, liquid hold-up, and cathode voltage, the catholyte feed solution should have a pH lower than about 10 and a buffer capacity to maintain the bulk catholyte pH less than 10 throughout the reaction. The CO$_2$(aq) concentration and pH at the reactive cathode surface depend on these bulk conditions, coupled with the current density and L/S mass transfer coefficient, as detailed in Reference 57. Considered along with the equilibria, these mass transfer and thermochemical reaction rates may favor the current density-dependent reduction of CO$_2$ to formate in the bulk pH range about 7–10 at 298 K. The changes in temperature that occur in a practical case will probably shift this pH window. Kinetic data are not available to calculate the effect of temperature, but applying the rule of thumb, that is, doubling of chemical reaction rates for 10 K increase in T, moves the upper limit of pH down from about 10 to 9 as temperature increases from 298 to 333 K. Apart from the above effects, the electrochemical kinetics of Reactions (3.1) and (3.2) play a major role in determining the formate CE over the whole pH range, and particularly at pH below about 6, where CO$_2$ sequestration as HCO$_3^-$/CO$_3^{2-}$ is not an issue.

As mentioned above, there exist overpotentials, or polarizations associated with the mass transport processes. For industrial electrochemical processes, the superficial current density and CE should be, respectively, at least 1 kA m$^{-2}$ and 50%. However, the relatively low solubility of CO$_2$ in aqueous solutions (ca. 70 mM at STP), coupled with the CO$_2$(aq)/HCO$_3^-$/CO$_3^{2-}$ equilibria, creates a mass transfer constraint on the reduction of CO$_2$. Due to this mass transfer resistance, the resultant current remains very low even at the most active electrocatalyst. The primary current density limits to a maximum value of the order 10 mA cm$^{-2}$ under the typical laboratory reaction conditions (one-phase flow, 2D cathode) with 100 kPa (abs) CO$_2$ pressure at 298 K. Several devices have been suggested to relieve the CO$_2$ mass transfer constraint, including operation at super-atmospheric pressure and/or subambient temperature, using a GDE or using a fixed-bed cathode while providing a “3-phase interface” for the reaction by sparging the cathode chamber with CO$_2$ gas [58–63].

### 3.4 KINETICS AND CATALYSIS OF CO$_2$ ELECTROREDUCTION

#### 3.4.1 Steps in CO$_2$ Electroreduction

As stated, most of the CO$_2$ electrocatalytic reduction on the surface of an electrode consists of several steps, including mass transfer of the reactants, surface reactions, interfacial charge transfer, and products involving bulk and surface diffusion, forming a complicated system whose components in those different processes affect each other. Each of them may give rise to a polarization phenomenon as discussed above. Figure 3.10 gives the plausible mass transfer at the electrode–electrolyte boundary layer.

Lack of exact rate constants makes the investigation of CO$_2$ electroreduction mechanisms even more difficult.
**3.4.2 Dynamic Influences On CO$_2$ Electroreduction**

CO$_2$ electrochemical reduction is a highly surface-sensitive reaction. The CO$_2$ coordinates to the metal via either a $\eta^1$ or $\eta^2$ bond depending upon the identity of the metal and its surface conditions [12,14], to give adsorbed carbon dioxide. The CO$_2$(ads) then accepts an electron to form the adsorbed radical species, $\cdot$CO$_2$(ads), as mentioned above, from which a number of reaction pathways are possible as discussed below.

In addition, the rates of CO$_2$ reduction can also be significantly affected within the system by electrolyte size and charge as well. For example, rates increased Cl$^-$ < Br$^-$ < I$^-$ for CO$_2$ reduction in MeOH/H$_2$O on Cu [64,65], and rates increased upon moving from Na$^+$ to La$^{3+}$ in an aqueous Cu system [64].

**3.4.3 Turnover Frequency Of CO$_2$ Hydrogenation**

The calculated turnover frequency (TOF), as a function of the oxygen adsorption energy, $\Delta E_0$, at ambient pressure and 500 K, is investigated as shown in Figure 3.11 [66]. The optimum in reaction rate is a result of competition between having a too weak interaction with oxygen, resulting in too unstable intermediates and high reaction barriers and a too strong coupling to oxygen, giving rise to surface poisoning by formate, and possibly other species bound through oxygen. As observed, elemental copper is closest to the top, whereas nickel and palladium bind oxygen too strongly and weakly, respectively. Zinc doping in a copper surface step, which can be used to model the active site of Cu/ZnO/Al$_2$O$_3$ industrial catalysts, [67], have close to
optimal activity. However, the density of such sites is small in a doped system [67], and a more homogeneous catalyst with the same activity per site but more active sites would be advantageous. The model, a good description either in theoretical or experimental view, provides a good starting point for discovering potential catalysts.

Generally, commercial electrochemical processes typically run at a turnover rate of about 1–10 per second.

### 3.4.4 Reaction Kinetics and Mechanism of CO₂ Electroreduction

#### 3.4.4.1 Metal Electrodes

Although there is no general consensus on the mechanism for hydrogenation at Cu/ZnO catalysts, Cu(I) sites are thought to promote catalytic activity and selectivity toward CH₃OH. Although Cu–Zn alloys are considered active sites for CO₂ reduction, Cu(I) sites are considered key species for CO adsorption in hydrogenation reactions [68]. Further, Cu(I) sites are believed to stabilize reaction intermediates such as carbonates (CO₃²⁻), formates (HCOO⁻), and methoxy adsorbates (H₃CO⁻) due to their higher heats of adsorption [69]. Sheffer et al. showed that alkali metals help stabilize Cu(I) active sites and increase Cu(I) concentrations which significantly improve CH₃OH yield [70]. Oxidation studies at single crystal Cu(I) shows that H₃CO adsorbed at (111) surfaces with Cu(I) atoms at the second atomic layer allows coordinately unsaturated oxygen anions to act as hydrogen abstraction sites.
for dehydrogenation [71]. In this case, it is possible that the unsaturated oxygen atoms at the (111) surfaces of the cuprous oxide film act as hydrogen donors sites in the reduction reaction.

A theoretical report by Peterson et al. describes a pathway for the electrochemical reduction of CO₂ to CH₄ at Cu electrodes based on density functional theory (DFT) and computational hydrogen electrode (CHE) models applied to Hori’s experimental data [72]. In that work, the authors indicate that the carbon atom of CO adsorbates may be hydrogenated via proton transfer to form HCO at −0.74 V (RHE). Hydrogenation of an adsorbed CO species is proposed to occur directly via proton addition from solution as their availability is significantly greater than hydrogenation from adsorbed hydrogen. Accordingly, once the HCO species is formed, the carbon atom continues proton and electron transfer reactions to form H₃CO adsorbates. Following this pathway, the last proton transfer to the H₂CO species (on Cu(211) surfaces) favors CH₄ formation by 0.27 eV. In the case of cuprous oxide electrodes as described here, the reduction reaction may benefit from both improved intermediate stability and the ability of H⁺ species coordinated with surface-bound oxygen. This surface would allow hydrogen addition to the oxygen atom of the H₂CO adsorbate rather than the carbon atom as shown in Figure 3.12 [73].

The formation of HCO⁻ intermediate has been reported as the r.d.s. in CO₂ reduction to CH₄, and H₂CO⁻ intermediate is detected in both hydrogenation and photoelectrocatalytic process for CH₃OH formation [72,74]. Two possible mechanism pathways (a and b) for the direct electrochemical reduction of CO₂ to CH₃OH at Cu/ZnO catalyst are proposed in Figure 3.13 [73]. Although mechanism (a) proceeds through CO pathway, mechanism (b) undergoes formate (HCOO⁻) intermediate. The last four steps in both (a) and (b) mechanism pathways are the same with HCO adsorbate formation, H₂CO adsorbate formation, H₃CO adsorbate formation, and hydrogenation of H₃CO adsorbate to CH₃OH.

Pathway (a) proceeds via CO intermediate, similar to Peterson and Gattrell’s mechanisms for CO₂ reduction at Cu surfaces [72,75]. The first electron and proton transfer may be associated with the formation of dioxymethylene (HOCO⁻). When another electron and proton are added to the OH group of the HOCO⁻ adsorbate, the C–OH₂ bond is broken to desorb a H₂O molecule and leave CO adsorbate on the surface. The reaction continues with the formation of HCO species by H addition to the C atom. Once the HCO species are formed, the carbon atom continues proton and electron transfer reactions to form H₂CO and H₃CO adsorbates. Although it is not

**FIGURE 3.12** Hydrogenation of methoxy adsorbates at Cu₂O(111) surfaces. (Le, M. T. H. *Electrochemical Reduction of CO₂ to Methanol*. Louisiana State University, 2011. Reproduced by permission of The Royal Society of Chemistry.)
clear whether these adsorbates would attach to the Cu, Zn, or O bond, ZnO (10–10) surface would promote CH₃OH formation by drawing OH adsorption and allowing the H atom to attach to the O atom of the H₃CO species. Pathway (b) proceeds via HCOO⁻ intermediate [74]. The H attaches to the C atom instead of the O atom on CO₂ adsorbate, hence, forming HCOO⁻ rather than HOCO⁻. The mechanism proceeds with H additions to the O atom of the formate (HCOO) species first to form HCO after an H₂O molecule dissociates from the surface. Similar to mechanism (a), once HCO species are formed, the reaction continues electron and proton transfer until CH₃OH is desorbed from the surface.

In Hg, Tl, Pb, In, Sn, and Cd at aqueous solution, the formation of HCOO⁻ may be initiated by one electron transfer to CO₂ at the potential negative of −1.6 V vs. SHE, forming ·CO₂⁻ present mostly freely in the solution close to the electrode as depicted in Figure 3.14 (1). The hydrogen bond by water molecules [76] and the high dielectric constant of water molecule contribute to the stabilization of ·CO₂⁻ in solution. The concentration of ·CO₂⁻ would be ca. 10⁻⁵ mol dm⁻³, if one takes into account the standard potential −1.85 V or −1.90 V and the Nernst relation 59 mV decade⁻¹ at 25°C. Free ·CO₂⁻ will take a proton at the nucleophilic carbon atom from a H₂O molecule.
Electrode Kinetics of CO₂ Electroreduction

acting as a Lewis acid, forming HCO₂. H⁺ will not be bonded to the O atom of -CO₂ because pKa value of the acid–base couple (-CO₂/CO₂H) is low at 1.4 [77]. HCO₂⁻ is subsequently reduced to HCOO⁻ at the electrode in aqueous media. The electrode potentials of Pb, Cd, and Tl are −1.6 V or more negative at 5.0 mA cm⁻² [31]. The potential of Hg is −1.51 V at 0.5 mA cm⁻², which would be equivalent to −1.7 V at 5.0 mA cm⁻² with an assumption of the transfer coefficient for HCOO⁻ formation 0.25 [5,9,65]. In nonaqueous media, H₂O molecule is not available and plenty of CO₂ is present. A CO₂ molecule will play a role of a Lewis acid with the nucleophilic C of -CO₂. The coupling of -CO₂ and CO₂ will lead to the formation of an adduct

FIGURE 3.14 Reaction scheme of the electrochemical reduction of CO₂. (Reproduced from the Electrochimica Acta, 39, Hori, Y. et al. Electrocatalytic process of CO selectivity in electrochemical reduction of CO₂ at metal electrodes in aqueous media, 1833–1839, Copyright 1994, with permission from Elsevier.)
intermediate \((\text{CO}_2)_2^-\), thus producing oxalate [76], which is more probable than Savéant’s coupling mechanism [78]. By contrast, CO is produced by a mechanism different from HCOO\(^-\) formation which may proceed with free -CO\(^2\)\(^-\) intervening. CO is favorably produced from the electrode metals which stabilize -CO\(^2\) effectively.

On the metal electrode surface of Au, Ag, Zn, Pd, Ga, or Cu, giving CO as the major product, -CO\(^2\) is stabilized by adsorption both in aqueous and nonaqueous electrolytes. Electrophilic reagents, H\(_2\)O in aqueous solution, react with the O atom of adsorbed -CO\(^2\), forming CO(ad) and OH\(^-\) as depicted in Figure 3.14 (2). H\(^+\) will not take part in the CO formation as the partial current of CO formation is independent of pH. CO(ad) is readily desorbed from the electrode as a gaseous molecule. The sequence of CO selectivity roughly agrees with that of the electrode potentials shown in Table 3.2. In nonaqueous media, a CO\(_2\) molecule reacts as a Lewis acid with adsorbed -CO\(^2\), and allows a C–O bond of the -CO\(^2\) to be broken. This process forms CO(ad) and -CO\(^2\) as postulated by Hammouche and his coworkers [79] for electrochemical reduction of CO\(_2\) catalyzed by iron porphyrins. CO(ad) thus formed is easily desorbed, as shown in Figure 3.14 (2). Cd, Sn, and In, of medium CO selectivity, do not strongly adsorb -CO\(^2\). -CO\(^2\) will be most freely present in aqueous electrolyte owing to the stabilization by water molecules over hydrogen bond [76] and the high dielectric constant. -CO\(^2\) stabilized in the electrolyte will be further reduced to HCOO\(^-\). However, -CO\(^2\) is not sufficiently stabilized in nonaqueous electrolyte due to lack of hydrogen bond formation and low dielectric constant of the solvents. Thus, -CO\(^2\) adsorbed on Cd, Sn, and In may be relatively more stable than -CO\(^2\) dissolved in the electrolyte. These metals yield CO in nonaqueous media in the same manner as Au, Ag, and Zn in Figure 3.14 (2). The CO selectivity mentioned above will be closely connected to the stability of adsorbed -CO\(^2\) on the electrode.

In H\(_2\)O–DMF solutions, the electrochemical reduction of CO\(_2\) at Pb and Hg give mainly oxalate or formate, depending on the concentration of H\(_2\)O, with scarce formation of CO at relatively low yield [80–82]. It is proposed that an electron transfer to CO\(_2\) molecule initiates the process, forming -CO\(^2\), which is not adsorbed on Pb, Hg, and Tl, and is freely present in nonaqueous electrolyte solution as well. And the interactions between the electrode and the reactants, intermediates, and products are negligible as the CO\(_2\) reduction at Hg and Pb electrodes proceeds at potentials close to the standard potential of -CO\(^2\)/CO\(_2\) couple. Several competing homogeneous reactions sequentially take place in parallel in the electrolyte solution (Figure 3.15). The product distribution at Pb and Hg electrodes is determined by the current density and the concentration of CO\(_2\) and H\(_2\)O [80]. Oxalate is formed by coupling of -CO\(^2\), Figure 3.15 (1), formate is formed in a way similar to that in aqueous electrolyte, Figure 3.15 (5)(5’), and CO is formed by sequential reactions (2) and (3) or (3’) in Figure 3.15.

3.4.4.2 Molecular Electrocatalysts

In the proposed mechanism of molecular catalyst of [Ni\(^{\text{II}}\)cyclam\(^2+\)] complex (structure 1, Figure 3.16), the [Ni\(^{\text{II}}\)cyclam\(^+\)] complex is assumed to play a crucial role as shown in Figure 3.17, and in particular, a [Ni\(^{\text{II}}\)cyclam(CO)]\(^+\) intermediate species has been detected in the course of selective electroreduction of CO\(_2\) to CO in aqueous solution. Fourteen-membered cyclam framework is a crucial prerequisite for the
Electrode Kinetics of CO₂ Electroreduction

(0) \[ \text{CO}_2 + e^- \rightleftharpoons \text{CO}_2^- \]

(1) \[ 2\text{CO}_2^- \rightarrow \text{CO} \cdot \text{OO} \cdot \text{CO} \cdot \text{O} \cdot \text{O} \cdot \text{CO}_2^- \]

(2) \[ \text{CO}_2^- + \text{CO}_2 \rightleftharpoons \text{CO} \cdot \text{O} \cdot \text{C} \cdot \text{O} \cdot \text{CO}_2^- \]

(3) \[ \text{O} \cdot \text{C} \cdot \text{O} \cdot \text{O}^- + e^- \rightarrow \text{CO} + \text{CO}_3^- \]

(3') \[ \text{O} \cdot \text{C} \cdot \text{O} \cdot \text{O}^- + \text{CO}_2^- \rightarrow \text{CO} + \text{CO}_3^- + \text{CO}_2 \]

(4) \[ \text{CO}_2^- + \text{H}_2\text{O} \rightleftharpoons \text{HCO}_2^- + \text{OH}^- \]

(5) \[ \text{HCO}_2^- + e^- \rightarrow \text{HCO}_2^- \]

(5') \[ \text{HCO}_2^- + \text{CO}_2^- \rightarrow \text{HCO}_2^- \]


[FIGURE 3.16 Molecular catalysts of transition metal complexes and nonmetal nitrogen-based pyridinium.]

1. [Ni]^{II}(cyclam)]^{2+}
2. [Pd(triphosphine)(CH₃CN)]^{2+}
3. Pyridinium

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Electrochemical Reduction of Carbon Dioxide

Encircled nickel center to act as catalyst in the CO₂ electroreduction. The planar ligand geometry of the Ni(cyclam), allowing access to the metal center, has been suggested to be of significance with respect to the catalytic ability exhibited. The system favors the formation of the NiI state \([83,84]\). \([\text{Ni(II)-cyclam}]\) is reportedly a very selective electrocatalyst for CO₂ reduction to CO and was found to catalyze carbon dioxide reduction on mercury electrodes at ca. 0.5 V below the calculated thermodynamic value \(E^0 = −0.41\) V vs. NHE at pH 5) at a “remarkable” velocity of ca. \(32 \text{ h}^{-1}\) with 95% CO formation CE. The catalyst was reported to cycle more than 1000 times with no notable deactivation. The system was found to be pH dependent, anion specific, prone to deactivation through CO buildup, resulting in Ni(cyclam)(CO) precipitation if the solution is not stirred and reported to require an Hg surface for appreciable rates and turnover \([85, 86]\).

As being developed to date, the most efficient catalyst of modified Fe-porphyrin \([87]\) with phenolic groups in all ortho and ortho’ positions on the phenyl groups \([88]\) as depicted in Figure 3.18 was reported to give CO in Faradaic yields >90% through \(5 \times 10^7\) turnovers over 4 h at an overpotential of just 0.465 V in DMF with 0.2 M water added causing no observable degradation. The enhancement in activity was attributed to the higher local concentration of protons associated with the phenolic hydroxyl groups.

For \([\text{Pd(triphosphine)(CH}_3\text{CN})]^{2+}\) catalysts (structure 2, Figure 3.16), the dissociation of a weakly coordinating solvent molecule of acetonitrile favors M–O bond formation during the electrocatalytic reduction cycle of CO₂ to CO. In addition,
Electrode Kinetics of CO$_2$ Electroreduction

Electron-donating substituents on the triphosphine ligand result in increased catalytic rates. The rate constant is between 5 and 300 M$^{-1}$ s$^{-1}$ [89]. The detail catalytic cycle is proposed as shown in Figure 3.19. As the Pd(II) complex gained an electron to form a Pd(I) intermediate, a reaction with CO$_2$ occurred to form a five-coordinate CO$_2$ adduct. Upon transfer of the second electron, the Pd(0) intermediate dissociated the solvent. Protonation of one of the oxygen atoms of coordinated CO$_2$ affords a metallo-carboxylic acid intermediate, Pd–COOH. It is believed that the metallo-carboxylic acid is protonated again to form a “dihydroxy carbene,” and that CO is then formed by dehydration of the dihydroxy carbene. CO dissociation and solvent association regenerates the initial complex. In solutions of high acid concentration, the r.d.s. was found to be the reaction of the Pd(I) intermediate with CO$_2$, though, in solutions of low acid concentrations, the cleavage of the C–O bond to form carbon monoxide and water limits the rate of the catalytic cycle. These classes of Pd phosphine complexes have shown catalytic rates in the range of 10–300 M$^{-1}$ s$^{-1}$ and with >90% CEs for CO production. Overpotentials were in the range of 100–300 mV, yet turnover numbers were low (ca. 10–100) and the decomposition to Pd(I) dimers and hydrides eventually causes cessation of catalytic activity [85,90,91].

Molecular CO$_2$ reduction catalyst of binuclear palladium complex (structure 3, Figure 3.16), in which two or more independent Pd triphosphine units Pd(P$_3$) are incorporated and separated by a methylene spacer, binds CO$_2$ through two Pd sites, with one metal interacting with C, the other with O. This complex palladium catalysts show very high catalytic rates, increasing by three orders of magnitude, for CO$_2$ reduction (>104 M$^{-1}$ s$^{-1}$), but with a turnover number of ca. 10. Along with this increase in catalytic activity came an increase in the formation of Pd(I)–Pd(I) bonds,
Electrochemical Reduction of Carbon Dioxide

thus decreasing catalyst lifetimes. And when the bridge spacer is not methylene, the dendrimers of the Pd catalyst showed decreased activity and selectivity [91].

Studies on the CO2 reduction to CO by the Re(bpy-R)(CO)3X system (R = H, Me, tBu, X = halogen, OTf, or a neutral ligand with a noncoordinating anion) [93] indicated that the complex undergoes a two-electron reduction and loses the labile X ligand to form an anionic tricarbonyl species (A), reported to be the active form of the catalyst, best described as a Re0(bpy–R)−1 species [94]. The subsequent mechanistic steps are depicted in Figure 3.20. An intermediate of carboxylate species (B) is formed upon reaction of carbon dioxide with the anion (A). The carboxylate species is protonated to form a carboxylic acid species (C), which could then react with a second proton to liberate water and produce a tetracarbonyl cationic intermediate (D). Although the exact order of addition of protons, addition of electrons, and loss of product remain undetermined, the ligand loss and subsequent transfer of electron density to the metal center have been reported as essential steps in the process [93]. The intermediate species involved in catalysis will likely depend on reduction potentials and pKa’s of the complexes compared with the applied potentials and pKa’s of the Brönsted acids available in solution. TOFs of the bpy-tBu system greater than 250 s−1 have been reported [93]. The increasing TOF, compared with that of relatively low value of 21.4 h−1 for Re(bpy)(CO)3Cl in DMF–H2O (9:1) solution, forming CO at −1.49 V vs SCE with CEs at 98% and excellent selectivity over H2 production [95], attributed to the inclusion of tertiary butyl groups at the 4,4’ positions of the bipyridyl ligand [93] and protic additives to the system [96]. To date, it is one of the best and most well-studied electrocatalyst system of CO2, still underway almost 30 years on [92].

Electrode Kinetics of CO$_2$ Electroreduction

The bipyridine complexes of ruthenium, Ru(bipy)(CO)$_2^{2+}$, were found to electrocatalytically reduce CO$_2$ to CO and HCOO$^-$ at $-1.40$ V vs. SCE, when water was present [97], by a two-electron reduction process as shown in Figure 3.21 [85,97]. Following the production of CO, a five-coordinate neutral complex is formed. In the presence of CO$_2$, the complex forms an $\eta^1$-CO$_2$ adduct of Ru(0), which can also be formed by addition of two equivalents of OH$^-$ to Ru(bipy)(CO)$_2^{2+}$. Addition of a proton forms the LRu(CO)(COOH) species which under acidic conditions (pH 6.0) gains another proton to lose water and regenerate the catalyst. Under basic conditions (pH 9.5), the catalyst may undergo a two-electron reduction with the participation of a proton to create HCOO$^-$ and regenerate the five-coordinate Ru(0) complex. The insertion and two-electron attack rely on interactions between the reduced complexes and CO$_2$ as the electrophile. In this case, both are activated by the occupation of the $\pi^*$ orbitals of bipyridine. The ligand-based reduction exerts a strong influence on reactivity as electron density at the metal center and in the metal hydride bond is reported as increased making them more susceptible to CO$_2$ attack. The system is

helpful to elucidate several of the key intermediates in the reduction of CO$_2$, though with low turnover numbers and low selectivity.

cis[Os(bpy)$_2$(CO)H][PF$_6$] reported by Bruce et al. [32] leads to associative activation of CO$_2$ in nonaqueous solution. At a platinum electrode, the reduction took place at −1.4 to −1.6 V (vs. a NaCl-saturated calomel electrode). The proposed mechanism is illustrated in Figure 3.22. The complex accepts two electrons to give the active species which reacts with CO$_2$, binding as an extra ligand, leading to coordination sphere expansion. There are different routes proposed where either the initial interaction with the catalyst results in the disproportionation or two of the direduced molecules may combine to give an uncharged complex and disproportionation products, CO and carbonate. In the experiments where water was present, for example, including trace water of less than 10 mM, they reported the incorporation of a proton into the intermediate direduced species, followed by combination to give formate or CO and hydroxide. The complex structure was investigated with the H found cis to the carbonyl being swapped for ligands of different sizes, H > CH$_3$ > CH$_2$–C$_6$H$_5$ > C$_6$H$_5$. It was seen that the rate constant for the reaction decreased with increasing size of this ligand. The trans structure was also trialed as a catalyst but the less sterically demanding configuration was less active. This highlighted the impact of relatively small differences in the molecular structure of the catalyst with a pronounced effect upon catalytic ability seen.

A dinuclear copper(I) complex incorporating pyridyl-like groups was reported to activate and convert CO$_2$ selectively into oxalate at only a very small applied potential of $-0.03$ V vs NHE, via a very different and effective catalytic cycle as seen in Figure 3.23. The electrocatalytic reduction of the copper(II) ion to copper(I) appears to be rate limiting, which occurs at a readily accessible potential, around 2 V less negative than that required for CO$_2$ reduction to $\cdot \cdot$CO$_2$ in acetonitrile on a glassy carbon electrode [98]. Two dinuclear direduced copper complexes are thought to form a tetranuclear complex with two bridging CO$_2$-derived oxalates which are subsequently released as Li$_2$C$_2$O$_4$ precipitate. The reduction of CO$_2$ in this system is found at a significantly less negative potential than that of dioxygen allowing the selective reduction of CO$_2$ from air. Unfortunately, this catalyst only completed six turnovers with 12 equivalents of oxalate formed in 7 h. So it cannot be considered suitable as a realistic catalyst, yet however is the most efficient route to oxalate in terms of overpotential reported to date [87].

Nonmetal nitrogen-based pyridinium cation (structure 4, Figure 3.16) catalyst [99,100] acts as one-electron shuttle to perform multiple-electron, multiple-proton reduction of CO$_2$ effectively in aqueous solution with Faradaic efficiencies of methanol observed ~30% at overpotentials of only ~0.2 V on metal electrode. When this pyridinium ion catalyst was anchored to a p-GaP electrode, this photochemical system yielded nearly 100% Faradaic efficiency of methanol at potential 0.3 V below the thermodynamic potential of $-0.52$ V vs SCE for the reaction at pH 5.2 [101]. The detailed mechanism of pyridinium-catalyzed CO$_2$ reduction in aqueous solution was proposed [99] as given in Figure 3.24. The 6e-reduced product of methanol was
Electrochemical Reduction of Carbon Dioxide


FIGURE 3.24  Overall proposed mechanism for the pyridinium-catalyzed reduction of CO₂ to various products of formic acid, formaldehyde, and methanol. (Reproduced with permission from Barton Cole, E. et al. Using a one-electron shuttle for the multielectron reduction of CO₂ to methanol: Kinetic, mechanistic, and structural insights. Journal of the American Chemical Society. 132(33), 11539–11551. Copyright 2010 American Chemical Society.)
through a pathway of a series of single-electron transfer rather than the typical multielectron charge transfer. At metal electrodes, formic acid and formaldehyde were observed to be intermediate products with the pyridinium radical playing a role in the reduction of both intermediate products. The r.d.s. of the aqueous system was reportedly determined as being the initial step, formation of the pyridinium–CO$_2$ radical.

Large NR$_4^+$ cations reportedly shift CO$_2$ reduction to more negative potentials and decrease the associated rate constant as their size increases. This is hypothesized to be the blocking effect of the compact layer of adsorbed cations, perhaps linked to the catalysis by tetraalkylammonium cations on CdTe in DMF and acetonitrile [102,103]. The catalysis was most greatly enhanced by the shorter alkyl chain length with NH$_4^+$ optimal. The supposed mechanism through which the enhancement was obtained was given as [103]:

1. NR$_4^+$ + e$^-$ → NR$_4^+$ (ads)
2. NR$_4^+$ (ads) + CO$_2$(ads) → NR$_4^+$ + CO$_2$(ads)
3. -CO$_2$(ads) + H$^+$ + e$^-$ → CO(ads) + OH$^-$
4. OH$^-$ + H$^+$ → H$_2$O

Upon addition of crown ether catalysts with ring structures in the solution, the tetraalkylammonium species, best able to fit within the cavity, yielded higher catalytic activity. The additional lowering of the overpotential in this case was thought to be a result of a similar mechanism as mentioned above, with the crown ether allowing the ammonium ion to get closer to the electrode surface, which is of specific adsorption in the inner Helmholtz plane, rather than outer Helmholtz, increasing the rate of electron transfer to the NR$_4^+$ species [103].

### 3.4.4.3 Electrocatalytic Activity Degradation

The reduction of CO$_2$ at Cu is inefficient, occurring at high overpotentials toward most probable products of hydrocarbons, and the activity drops rapidly as well [4,104–107]. The proposed mechanisms for the activity degradation include adsorption of organic intermediate [105,106], black carbon deposition [105,108], poison of copper oxide patina [107], accumulation of an unknown low vapor pressure and soluble CO$_2$ reduction product [109], and contaminants Fe$^{2+}$ and Zn$^{2+}$ deposition [4]. However, the real reason behind this is still unclear. The formation mechanism [110] of hydrocarbons [111] is still of a great challenge, though a good start of simulating elements of the reaction mechanism on Cu using DFT [72,112,113]. It is worth noting that Cu electrodes containing a Cu$_2$O surface layer demonstrated high activity toward CH$_3$OH production [114,115]. Cu(I) species was considered to play a critical role in the activity of CH$_3$OH formation. CH$_3$OH yielded qualitatively follow Cu(I) concentrations.

### 3.5 PRODUCT DISTRIBUTION AND COMPETITIVE REDUCTION BETWEEN CO$_2$ AND SOLVENT

#### 3.5.1 Product Distribution

There is a variety of possible product distributions as various pathway steps are involved in different experimental conditions, though a preference occurs for special
occasion. It is noted that small changes can lead to competitive reactions and different routes. Those make generalizations based on individual studies very dubious and grouping difficult.

The reduction product at an electrode in aqueous electrolytes depends on anionic and cationic species of the electrolyte solution, the applied potential, and temperature as discussed. It is reported that CO and HCOO\(^{-}\) were preferentially produced at less negative potentials of \(> -0.4 \text{ V vs. Ag/AgCl}\), whereas CH\(_4\), C\(_2\)H\(_4\), and C\(_2\)H\(_5\)OH were major products at the potential \(< -0.4 \text{ V vs. Ag/AgCl}\). The origin of the selectivity was hypothesized to relate to the special affinity of hydrogen and/or proton to electrodes. For example, at more negative potential, protons are so abundant on the electrode surface that adsorbed hydrogen-containing carbon molecules are preferentially formed on an Ag electrode. As a result, hydrocarbonization reactions between H\(_{\text{ad}}\) and CO\(_2\) are possible, yielding CH\(_4\), C\(_2\)H\(_4\), and C\(_2\)H\(_5\)OH. On the contrary, at a less negative potential, desorption of H\(_{\text{ad}}\) occurs, and adsorbed protons are not abundant enough to promote hydrocarbonization reactions. In this case, CO and HCOO\(^{-}\) are preferentially produced.

3.5.2 Competitive Reduction between CO\(_2\) and Solvent

Higher pH solution increases the presence of “H” on the electrode and the amount of carbon dioxide in solution; therefore, electrodes with low affinity for hydrogen adsorption such as aluminum will exhibit optimum CO\(_2\) reduction kinetics at high pH but for others (e.g., palladium) the stronger M–H bonds will mean that H(ads) will dominate the electrode surface, inhibiting CO\(_2\) reduction.

In general, to promote CO\(_2\) reduction reaction while suppressing the competing HER, an electrocatalyst capable of mediating multiple electron and proton transfers at relatively low overpotentials is desirable [111,116–118].

In, Sn, Hg, and Pb electrodes, all have high overpotential for H\(_2\) evolution, and negligible CO adsorption. In aqueous electrolyte, formic acid/formate is selectively produced with Faradaic efficiency between 70% and 100% [23,58,61,119–121].

d group metals (e.g., Pt, Pd, Ru, Fe, Cr, Mo, Ti, Nb, and Ni) have low activity to CO\(_2\) reduction while H\(_2\) evolution dominates. For example, on Ni electrodes, only CO, HCOOH, CH\(_4\), and C\(_2\)H\(_4\) with Faradaic efficiency less than 1% were detected in the aqueous electrolyte [120]. On Pd electrodes, CO and HCOOH are the main products from CO\(_2\) reduction, with maximum Faradaic efficiency <30% for both products [31,120]. Under high pressure, for example, 30 atm, the Faradaic efficiency of CO and HCOOH became comparable with that of H\(_2\) [122]. Interestingly, small yield of methanol was reported on Ru electrode [123,124]. Reduction of CO\(_2\) on alloy Ru–Pd (1:1) mainly produced HCOOH with a maximum Faradaic efficiency of 90% [125]. CO\(_2\) is reduced to adsorbed CO (CO\(_{\text{ad}}\)) on Pt catalysts, the activity of which remarkably depends on the symmetry of the single crystal surface. The following activity series are obtained for stepped surfaces: Pt(111) < Pt(100) < Pt(S) – [n(111) × (100)] < Pt(S) – [n(100) × (111)] < Pt(S) – [n(111) × (111)] < Pt(110). The initial rate of the CO\(_2\) reduction gets higher with the increase of the step atom density [126]. Moreover, kinked step surfaces, which contain protruding atoms along the step lines, have higher activity for CO\(_2\) reduction than the stepped surfaces [127].
The dominance of H₂ evolution could be shifted to CO₂ reduction on d group electrodes by increasing the pressure [120,122]. The formation of hydrocarbons on Cu electrode decreased upon increasing pressure [122,128], whereas lowering the temperature improved the hydrocarbons formation [60,105,120,129,130].

Figure 3.25 shows a result of controlled potential reduction of CO₂ at a Cu electrode in 0.1 M KHCO₃. The Faradaic yield of HCOO⁻, which is thought to be the precursor of the final product of hydrocarbons/alkohols and not reduced at all at a Cu electrode, rises at −0.9 V, reaching maximum at −1.20 to −1.25 V, and drops with the increase of the cathodic potential, whereas H₂ is formed at lower potential with decreasing Faradaic yield along the line.

As shown in Table 3.6, KHCO₃, KCl, KClO₄, and K₂SO₄ solutions favor the CO₂ reduction. K₂HPO₄ solutions highly promote HER rather than CO₂ reduction at less negative potential. 0.5 M K₂HPO₄ gives much higher H₂ yields than 0.1 M K₂HPO₄. Such an enhancement of HER is attributed to lower pH value at the electrode/electrolyte interface, as mentioned previously. The pH would rise locally at the interface due to OH⁻ generation in cathodic reactions in aqueous media. Nevertheless, the buffer action of HPO₄²⁻ neutralizes the OH⁻, keeping the pH at a lower value. KCl, KClO₄, and K₂SO₄ solutions do not have buffer ability, and thus the pH at the electrode/electrolyte interface rises. HER goes up with the concentration of KHCO₃ as indicated in Figure 3.26, owing to its buffer action.

In an ionic liquid catholyte of 1-ethyl-3-methyl imidazolium tetrafluoroborate (EMIM-BF₄), the conversion of CO₂ to CO over Ag GDE (Figure 3.27) showed substantial improvement over both Faradaic efficiency (~100%) and the overpotential less negative than −0.2 V toward CO formation [29]. The ionic liquid was considered to react with CO₂ to form a complex such as CO₂–EMIM at potentials more negative
# TABLE 3.6
Faradaic Efficiencies of Products from the Electroreduction of CO₂ at a Cu Electrode at 5 mA cm⁻² in Various Solutions at 19°C

<table>
<thead>
<tr>
<th>Solution</th>
<th>Concentration, M</th>
<th>pH</th>
<th>Potential V vs. SHE</th>
<th>CH₄</th>
<th>C₂H₄</th>
<th>EtOH</th>
<th>PrOH</th>
<th>CO</th>
<th>HCOO⁻</th>
<th>H₂</th>
<th>Total</th>
</tr>
</thead>
<tbody>
<tr>
<td>KHCO₃</td>
<td>0.1</td>
<td>6.8</td>
<td>−1.41</td>
<td>29.4</td>
<td>30.1</td>
<td>6.9</td>
<td>3.0</td>
<td>2.0</td>
<td>9.7</td>
<td>10.9</td>
<td>92.0</td>
</tr>
<tr>
<td>KCl</td>
<td>0.1</td>
<td>5.9</td>
<td>−1.44</td>
<td>11.5</td>
<td>47.8</td>
<td>21.9</td>
<td>3.6</td>
<td>2.5</td>
<td>6.6</td>
<td>5.9</td>
<td>99.8</td>
</tr>
<tr>
<td>KCl</td>
<td>0.5</td>
<td>−1.39</td>
<td></td>
<td>14.5</td>
<td>38.2</td>
<td>b</td>
<td>b</td>
<td>3.0</td>
<td>17.9</td>
<td>12.5</td>
<td></td>
</tr>
<tr>
<td>KClO₄</td>
<td>0.1</td>
<td>5.9</td>
<td>−1.40</td>
<td>10.2</td>
<td>48.1</td>
<td>15.5</td>
<td>4.2</td>
<td>2.4</td>
<td>8.9</td>
<td>6.7</td>
<td>96.0</td>
</tr>
<tr>
<td>K₂SO₄</td>
<td>0.1</td>
<td>5.8</td>
<td>−1.40</td>
<td>12.3</td>
<td>46.0</td>
<td>18.2</td>
<td>4.0</td>
<td>2.1</td>
<td>8.1</td>
<td>8.7</td>
<td>99.4</td>
</tr>
<tr>
<td>K₂HPO₄</td>
<td>0.1</td>
<td>6.5</td>
<td>−1.23</td>
<td>17.0</td>
<td>1.8</td>
<td>0.7</td>
<td>tr</td>
<td>1.3</td>
<td>5.3</td>
<td>72.4</td>
<td>98.5</td>
</tr>
<tr>
<td>K₂HPO₄</td>
<td>0.5</td>
<td>7.0</td>
<td>−1.17</td>
<td>6.6</td>
<td>1.0</td>
<td>0.6</td>
<td>0.0</td>
<td>1.0</td>
<td>4.2</td>
<td>83.3</td>
<td>96.7</td>
</tr>
</tbody>
</table>


*a* pH values were measured for bulk solution after electrolysis.

*b* Not analyzed.

Electrochemical Reduction of Carbon Dioxide

than $-0.1 \text{ V}$ with respect to SHE. This complex substantially lowered the barrier for formation of the intermediate $\cdot \text{CO}_2$ and suppressed $\text{H}_2$ evolution [131].

For MoS$_2$ catalysts in the electrolyte of 96 mol% water and 4 mol% EMIM-BF$_4$ at applied potentials between $-0.2$ and $-0.764 \text{ V}$, both CO$_2$ reduction to CO and HER on the electrode surface are observed as shown in Figure 3.28 [132]. The measured FE of the CO and $\text{H}_2$ formation, ranging from 0% to ~100% in each component, strongly depends on the applied potential, probably attributed to the difference in the mechanisms of CO$_2$ reduction and HER. At low overpotential, $\text{H}_2$ is predominantly produced as the favorable thermodynamic potential for the $\text{H}_2$ evolution is low compared with CO$_2$ reduction. However, when the applied potential exceeds the onset potential of $-0.164 \text{ V}$ at this system for the CO$_2$ reduction, CO$_2$ reduction reaction is activated and dominated instead of HER, in which two $\text{H}^+$ from the electrolyte per one CO$_2$ molecule reduction are consumed for CO formation, coupled with the electron transfer on the catalyst surface [40,75,133,134].

3.6 SUMMARY AND CHALLENGES

Although the electrochemical conversion of CO$_2$ has great potential, significant technological advances are still needed for this process to become economically viable. There are three criteria [135]: (1) high energy efficiency, (2) high current density (i.e., high reaction rate or turnover number), and (3) long-term stability. So far, the development of electrochemical reduction of CO$_2$ system is slow due to the lack of scientific understanding of CO$_2$ reduction mechanism (C–O, C–C, and C–H bonds formation), pathways and intermediates to generate useful products, providing insights into the CO$_2$ reduction chemistry at the electrode/electrolyte interface and the degradation mechanism of Faradaic efficiency, although some attempts to

**FIGURE 3.28** CO and $\text{H}_2$ Faradaic efficiency at different applied potentials for bulk MoS$_2$ in CO$_2$-saturated 96 mol% water and 4 mol% EMIM-BF$_4$ solution ($\text{pH} = 4$). (Reproduced by permission from Macmillan Publishers Ltd. *Nature Communications*, Asadi, M. et al. Robust carbon dioxide reduction on molybdenum disulphide edges. 5: 4470, copyright 2014.)
Electrode Kinetics of CO₂ Electroreduction

understand the CO₂ electroreduction process through both experimental and theoretical modeling approaches. Such efforts in fundamental mechanistic studies will guide the development of new catalysts and the optimization of operating conditions.

High energetic efficiency can be achieved through a combination of high selectivity (Faradaic or CE) and low overpotentials (Figure 3.29).

Typically, the Faradaic efficiency for many products is >90% for formic acid and carbon monoxide, 65%–70% for methane and ethylene, respectively. High overpotentials are a major hindrance to improving energy efficiency. The reaction rate, as measured by the current density, is also an important parameter as it determines the reactor size and thus capital cost of the process. To date, researchers have reported moderate-to-high current densities (200–600 mA/cm²) using GDEs similar to those used in fuel cells.

The limiting step in the reduction of CO₂ is the formation of a CO₂⁻ radical anion intermediate. (In this context, “CO₂⁻” does not necessarily denote a bare CO₂⁻ anion; instead, it is whatever species forms when an electron is added to CO₂.) The equilibrium potential for CO₂⁻ formation is very negative in water and in most common solvents [103,136] as discussed above, and this is the reason for the high overpotentials [11,29]. This potential can be improved by stabilizing the intermediate, which is one of the main functions of catalysts. Research has shown that the potential to form this radical anion can be improved by 0.3 V by adsorbing it on a catalyst surface [11]. Further improvements could be possible through optimization of the catalyst.

Another key limiting factor in CO₂ conversion is mass transfer of CO₂ to the cathode surface, especially given the low solubility of CO₂ in many electrolytes. As mentioned earlier, this has largely been overcome using GDEs, which create a three-phase interface between the gaseous reactants, the solid catalyst, and the electrolyte.

![Reaction coordinate](image)

**FIGURE 3.29** Qualitative reaction scheme for CO₂ conversion. Catalysts and electrolytes acting as cocatalysts can lower the energy of the intermediate and thus improve the energetic efficiency of the conversion. We use ε as the symbol for the Faradaic and energetic efficiencies to avoid confusion with the η symbol for the overpotential. (Reproduced with permission from Whipple, D. T. and Kenis, P. J. A. Prospects of CO₂ utilization via direct heterogeneous electrochemical reduction. *The Journal of Physical Chemistry Letters.* 1(24), 3451–3458. Copyright 2010 American Chemical Society.)
Thus, optimization of the electrode will be a key to improving current densities. The extensive work on GDE optimization for fuel cells over the past decades will greatly accelerate progress in this area.

Although remarkable achievements have been made in electrochemical reduction of CO$_2$ in the past two decades, there is limited scientific knowledge about CO$_2$ catalytic reduction. Due to the complexity of the reaction environment and multiple bond-forming and breaking processes, the detailed knowledge about the elementary pathways is obscured, which results in the difficulty in understanding the reaction kinetics and controlling the reaction chemistry. The determination of the transient catalytic intermediates is still not possible because of their very short lifetimes and low concentrations as well as difficulty in resolving intermediates spectroscopically. The characterization of surface intermediates under working conditions will require the development and application of sensitive ultrafast spectroscopic and pump-probe scattering methods. Coupling with the experimental probing, theoretical modeling, such as ab initio methods and DFT, is needed to calculate the overall reaction energies and activation barriers, which subsequently lead to construct overall potential energy surfaces. However, so far, simulating reaction conditions that explicitly treat the effects of surface coverage, electrolyte, electrochemical potential, and appropriate materials property, including the effects of particle size, surface orientation, and morphology, present significant challenges.

More work is needed to further understand the competition between H$_2$ evolution reaction and hydrogen protonation process. Multiphysical modeling is required to understand the ion (especially H$^+$) distribution across the buffer layer, the effect of electrolyte circulating rate, cell temperature and reaction gas pressure on the performance.

REFERENCES


